

CORE ANALYSIS REPORT
FOR
ELK OIL COMPANY
KELLS STATE NO. 1
SOUTH ACME FIELD
CHAVES COUNTY, NEW MEXICO

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CORE LABORATORIES

April 12, 1993

ELK OIL COMPANY
P.O. Box 310
Roswell, New Mexico 88202-0310

File No.: 57181-16760
Subject: Core Analysis
Kells State No. 1
South Acme San Andres Field
Chaves County, New Mexico

Gentlemen:

The subject well was cored using diamond coring equipment and stable foam to obtain 4 inch diameter cores from 2130 to 2190 feet from the San Andres formation.

Core analysis data is presented in tabular and graphical form for your convenience. A porosity vs. permeability plot and porosity and permeability histograms were prepared for statistical evaluation.

We trust these data will be useful in the evaluation of your property and thank you for the opportunity of serving you.

Very truly yours,

CORE LABORATORIES, a division of
WESTERN ATLAS INTERNATIONAL, INC.

Dean Olson
Laboratory Supervisor

DO/yn

ELK OIL COMPANY
Kells State No. 1
File No. 57181-16760
Procedural Page

The cores were preserved at the wellsite in CO₂ atmosphere and transported to Midland by Core Laboratories personnel.

A Core Gamma Log was recorded for downhole E-log correlation.

Core analysis was made from selected intervals requested on full diameter samples.

Fluid removal was achieved using a gas solvent extraction method.

Fluid saturations were determined using controlled temperature downdraft retort technique.

Porosity was determined by direct pore volume measurement using Boyle's law helium expansion. Bulk volume was measured by Archimedes Principle. Grain density was calculated from dry weight, bulk volume and pore volume measurements.

$$\text{Grain Density} = \frac{\text{Dry Weight}}{\text{Bulk Vol.} - \text{Pore Vol.}}$$

Steady State Air Permeability was measured in two horizontal directions while the core was confined in a Hassler rubber sleeve.

Vertical permeabilities were ran on selected samples.

The core was boxed and will remain at our Midland facility (thirty days free of charge) as we await further disposition instructions.

CORE LABORATORIES

ELK OIL COMPANY
 KELLS STATE NO. 1
 990' FNL & 330' FEL, SEC. 14, T-8-S, R-27-E
 CHAVES COUNTY, NEW MEXICO

Field : SOUTH ACME SAN ANDRES FIEL
 Formation : SAN ANDRES
 Coring Fluid : STABLE FOAM
 Elevation : 3939' GL

File No.: 57181-16760
 Date : 3-20-93
 API No. :
 Analysts: OLSON

C O R E A N A L Y S I S R E S U L T S

SAMPLE NUMBER	DEPTH ft	PERMEABILITY			POROSITY (HELIUM) %	SATURATION		GRAIN DENSITY gm/cc	DESCRIPTION
		(MAXIMUM) Kair md	(90 DEG) Kair md	(VERTICAL) Kair md		(PORE VOLUME) OIL %	WATER %		
CORE NO. 1 2130-2190 CUT 60' REC 59'									
1	2130.0- 31.0	2.41	2.06		6.9	19.8	27.2	2.85	Dol sli/any f styl
2	2131.0- 32.0	2.17	1.52		4.2	23.9	33.6	2.85	Dol sli/any F styl
3	2132.0- 33.0	0.96	0.04		4.4	7.9	48.2	2.85	Dol sli/any vf styl
4	2133.0- 34.0	1.29	0.47		3.9	33.0	20.5	2.85	Dol sli/any vf styl
5	2134.0- 35.0	0.44	0.15		2.9	35.3	30.9	2.84	Dol sli/any vf
6	2135.0- 36.0	0.43	0.06	0.07	3.5	28.2	24.7	2.86	Dol F styl
7	2136.0- 37.0	2.77	0.46	0.25	5.3	19.3	32.1	2.85	Dol sli/any vf p.p.
8	2137.0- 38.0	0.06	0.06	9.42	1.0	34.9	36.1	2.81	Dol sli/shy vf styl
9	2138.0- 39.0	0.06	0.03	4.96	0.8	52.1	31.3	2.82	Dol sli/shy vf styl
10	2139.0- 40.0	4.16	3.78	79.6	10.7	9.9	21.0	2.84	Dol vf sli/vug
11	2140.0- 41.0	1.20	0.14	1.06	11.6	11.3	26.8	2.84	Dol any vug
12	2141.0- 42.0	0.89	0.66	0.23	11.6	15.9	13.7	2.86	Dol any vf p.p.
13	2142.0- 43.0	42.5	2.07	1.97	3.5	29.9	24.9	2.84	Dol F vf styl
14	2143.0- 44.0	49.4	0.04	884.	2.4	22.0	66.0	2.81	Dol sli/any vf sli/vug
15	2144.0- 45.0	0.06	0.02	43.4	7.2	10.0	36.7	2.85	Dol vf p.p.
16	2145.0- 46.0	1.25	0.29	2.52	8.3	21.3	23.6	2.84	Dol vf p.p.
17	2146.0- 47.0	0.33	0.32	0.05	4.8	21.4	25.0	2.85	Dol vf sli/vug
18	2147.0- 48.0	6.15	2.95	0.84	4.4	12.0	35.1	2.85	Dol sli/any vf sli/vug styl
19	2148.0- 49.0	0.81	0.19		1.8	24.6	41.0	2.84	Dol f styl
20	2149.0- 50.0	83.5	36.0		2.1	25.7	21.4	2.85	Dol sli/any vf vug styl
21	2150.0- 51.0	40.7	8.29		4.5	8.5	38.8	2.84	Dol vf styl
22	2151.0- 52.0	14.9	10.3	6.44	2.3	35.8	28.7	2.84	Dol vf
23	2152.0- 53.0	5.85	3.32	0.34	5.0	7.1	49.4	2.84	Dol sli/any vf
24	2153.0- 54.0	34.0	0.12	4.11	4.7	5.8	46.0	2.84	Dol vf
25	2154.0- 55.0	320.	0.34	133.	4.0	16.7	53.1	2.80	Dol vf

CORE LABORATORIES

ELK OIL COMPANY
KELLS STATE NO. 1

Field : SOUTH ACME SAN ANDRES FIELD
Formation : SAN ANDRES
File No.: 57181-16760
Date : 3-20-93

CORE ANALYSIS RESULTS

SAMPLE NUMBER	DEPTH ft	PERMEABILITY			POROSITY (HELIUM) %	SATURATION		GRAIN DENSITY gm/cc	DESCRIPTION
		(MAXIMUM) Kair md	(90 DEG) Kair md	(VERTICAL) Kair md		(PORE VOLUME) OIL %	WATER %		
* 26	2155.0- 56.0		0.01		3.3	5.7	35.5	2.89	Dol anhy F p.p.
27	2156.0- 57.0	52.5	40.5	6.58	5.7	16.2	26.3	2.84	Dol sli/anhy vf sli/vug
28	2157.0- 58.0	52.4	10.7	7.87	8.5	23.7	30.6	2.85	Dol sli/anhy vf sli/vug
* 29	2158.0- 59.0		0.01		3.5	12.5	22.7	2.87	Dol anhy F p.p.
30	2159.0- 60.0	490.	392.	0.28	8.9	14.9	26.0	2.85	Dol sli/anhy vf sli/vug styl
31	2160.0- 61.0	166.	61.6	18.7	8.2	14.8	25.2	2.86	Dol sli/anhy vf p.p.
32	2161.0- 62.0	424.	90.3	3.61	7.1	21.0	26.2	2.85	Dol sli/anhy vf p.p.
33	2162.0- 63.0	86.8	33.5	24.4	6.7	18.8	37.6	2.84	Dol sli/anhy vf vug
34	2163.0- 64.0	21.1	11.5	0.47	5.3	5.6	35.3	2.85	Dol sli/anhy vf p.p. styl
35	2164.0- 65.0	5.87	1.62	0.75	7.9	4.3	42.7	2.85	Dol sli/anhy vf p.p. styl
36	2165.0- 66.0	202.	45.8	25.7	11.3	4.5	41.1	2.84	Dol vf p.p. styl
37	2166.0- 67.0	19.8	9.73	3.27	2.9	16.6	33.1	2.84	Dol vf
38	2167.0- 68.0	174.	157.	5.28	5.6	10.9	36.4	2.86	Dol anhy vf styl
39	2168.0- 69.0	138.	108.	10.9	6.4	7.9	35.2	2.85	Dol sli/anhy vf
40	2169.0- 70.0	47.6	42.0	2.83	5.3	16.6	16.6	2.85	Dol sli/anhy vf
41	2170.0- 71.0	25.9	14.5		3.4	23.0	26.1	2.85	Dol sli/anhy vf styl
42	2171.0- 72.0	36.2	13.5		2.8	10.8	35.9	2.84	Dol f styl
43	2172.0- 73.0	2.69	0.79		3.7	15.8	28.5	2.85	Dol sli/anhy f styl
44	2173.0- 74.0	5.84	2.15		3.2	3.9	39.4	2.85	Dol sli/anhy f styl
45	2174.0- 75.0	0.67	0.50		1.0	0.0	74.1	2.86	Dol anhy f styl
46	2175.0- 76.0	1.94	<.01		1.4	2.4	48.2	2.87	Dol anhy vf
47	2176.0- 77.0	22.4	5.27		1.2	5.2	77.4	2.86	Dol anhy vf styl
48	2177.0- 78.0	0.05	0.03		0.7	0.0	72.7	2.85	Dol sli/anhy vf styl
	2178.0- 89.0								NA Anhy - Removed by client
	2189.0- 90.0								Lost core

* INDICATES PLUG PERMEABILITY

CORE LABORATORIES

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 KELLS STATE NO. 1
 990' FNL & 330' FEL, SEC. 14, T-8-S, R-27-E
 CHAVES COUNTY, NEW MEXICO

Field : SOUTH ACME FIELD
 Formation : SAN ANDRES
 Coring Fluid : STABLE FOAM
 Elevation : 3939' GL

File No.: 57181-16760
 Date : 3-21-93
 API No. :
 Analysts: OLSON

CORE ANALYSIS RESULTS

SAMPLE NUMBER	DEPTH ft	POROSITY (FLUIDS) %	SATURATION		FLU	DESCRIPTION
			(PORE VOLUME) OIL %	WATER %		

SUMMATION OF FLUIDS DATA

1	2130.0- 31.0	4.1	21.4	29.5	70.	Dol sli/anyh styl
2	2131.0- 32.0	8.1	9.5	13.4	50.	Dol sli/anyh F styl
3	2132.0- 33.0	1.9	11.6	70.8	50.	Dol sli/anyh vf styl
4	2133.0- 34.0	2.3	43.2	26.9	60.	Dol sli/anyh vf styl
5	2134.0- 35.0	5.0	17.4	15.2	25.	Dol sli/anyh vf
6	2135.0- 36.0	6.1	13.9	12.2	80.	Dol F styl
7	2136.0- 37.0	9.2	10.1	16.9	70.	Dol sli/anyh vf p.p.
8	2137.0- 38.0	2.8	46.9	48.5	20.	Dol vf styl shale-oil
9	2138.0- 39.0	2.3	46.9	28.1	20.	Dol vf sli/vug
10	2139.0- 40.0	13.9	6.3	13.3	30.	Dol vf sli/vug
11	2140.0- 41.0	11.7	8.0	19.2	50.	Dol sli/anyh vug
12	2141.0- 42.0	2.2	34.7	29.8	70.	Dol vf p.p.
13	2142.0- 43.0	1.5	45.7	38.1	50.	Dol F vf styl
14	2143.0- 44.0	2.2	10.1	30.4	50.	Dol sli/anyh vf vug
15	2144.0- 45.0	8.1	7.8	28.6	70.	Dol vf p.p.
16	2145.0- 46.0	4.7	20.3	22.5	70.	Dol vf p.p.
17	2146.0- 47.0	3.1	21.2	24.8	20.	Dol vf sli/vug
18	2147.0- 48.0	1.3	20.7	60.5	20.	Dol sli/anyh vf vug styl
19	2148.0- 49.0	1.6	20.9	34.9	20.	Dol f styl
20	2149.0- 50.0	1.0	32.3	26.9	20.	Dol sli/anyh vf vug styl
21	2150.0- 51.0	5.8	5.1	23.2	10.	Dol vf styl
22	2151.0- 52.0	2.2	32.2	25.8	10.	Dol vf shale-oil
23	2152.0- 53.0	6.8	3.9	27.2	10.	Dol sli/anyh vf
24	2153.0- 54.0	3.4	8.1	64.9	2.	Dol vf
25	2154.0- 55.0	1.7	18.4	58.5	10.	Dol vf

CORE LABORATORIES

ELK OIL COMPANY
KELLS STATE NO. 1

Field : SOUTH ACME FIELD
Formation : SAN ANDRES

File No.: 57181-16760
Date : 3-21-93

C O R E A N A L Y S I S R E S U L T S

SAMPLE NUMBER	DEPTH ft	POROSITY (FLUIDS) %	SATURATION		FLU	DESCRIPTION
			(PORE VOLUME) OIL %	WATER %		
26	2155.0- 56.0	3.3	8.4	52.2	2.	Dol F p.p.
27	2156.0- 57.0	15.8	11.8	19.2	20.	Dol sli/anhy vf sli/vug
28	2157.0- 58.0	24.6	14.6	18.9	20.	Dol sli/anhy vf sli/vug
29	2158.0- 59.0	3.8	8.0	14.6	2.	Dol F p.p.
30	2159.0- 60.0	7.3	14.9	26.1	5.	Dol vf sli/vug styl
31	2160.0- 61.0	6.6	20.9	35.5	10.	Dol sli/anhy vf p.p.
32	2161.0- 62.0	9.3	22.4	27.9	10.	Dol vf p.p.
33	2162.0- 63.0	1.5	18.0	35.9	20.	Dol vf vug
34	2163.0- 64.0	6.7	4.4	28.1	10.	Dol sli/anhy vf p.p. styl
35	2164.0- 65.0	9.8	3.2	32.0	10.	Dol sli/anhy vf p.p. styl
36	2165.0- 66.0	7.5	4.3	39.2	10.	Dol vf p.p. styl
37	2166.0- 67.0	4.4	9.4	18.8	5.	Dol vf
38	2167.0- 68.0	4.7	8.6	28.8	10.	Dol anhy vf styl
39	2168.0- 69.0	8.6	7.7	34.6	20.	Dol sli/anhy vf
40	2169.0- 70.0	4.5	21.3	21.3	50.	Dol vf
41	2170.0- 71.0	1.4	29.8	33.7	30.	Dol vf styl shale-oil
42	2171.0- 72.0	4.4	9.4	31.2	20.	Dol f styl
43	2172.0- 73.0	3.7	18.7	33.6	5.	Dol sli/anhy styl
44	2173.0- 74.0	1.3	4.2	42.5	10.	Dol sli/anhy styl
45	2174.0- 75.0	0.6	0.0	49.3	0.	Dol f styl
46	2175.0- 76.0	0.8	3.3	66.9	0.	Dol vf
47	2176.0- 77.0	0.8	3.7	56.2	0.	Dol vf
48	2177.0- 78.0	0.8	0.0	74.3	0.	Dol vf styl

LITHOLOGICAL ABBREVIATIONS

Anhy, anhy	anhydrite (-ic)	Lim, lim	limestone
Ark, ark	arkose (-ic)	med gr	medium grain
bnd	band (-ed)	Mtrx	matrix
Brec, brec	breccia	NA	interval not analyzed
Calc, calctc	calcite (-ic)	Nod, nod	nodules (-ar)
carb	carbonaceous	Ool, ool	oolite (-itic)
crs gr	course grained	Pisol, pisol	pisolite, pisolitic
Chk, chky	chalk (-y)	p.p.	pin-point (porosity)
Cht, cht	chert (-y)	Ptg	parting
Ogl, ogl	conglomerate (-ic)	Pyr, pyr	pyrite (-itized, -itic)
crs xln	coarsely crystalline	Sd, sdy	sand (-y)
dns	dense	Sh, shy	shale (-ly)
Dol, dol	dolomite (-ic)	SHR	solid hydrocarbon residue
F	randomly oriented fractures	sli	slightly
f	slightly fractured	Slt, slty	silt (-y)
f gr	fine grained	styl	stylolite (-itic)
foss	fossil (-iferous)	suc	sucrosic
f xln	finely crystalline	Su, su	sulphur, sulphurous
Gil	gilsonite	TBFA	TOO BROKEN FOR ANALYSIS
Glauc, glauc	glauconite (-itic)	Trip, trip	tripoli (-itic)
Grt	granite	v	very
Gyp, gyp	gypsum (-iferous)	vf	predominantly vertically fractured
hor frac	predominantly horizontally fractured	vug	vug (-gy)
incl	inclusion (-ded)	xbd	crossbedded
intbd	interbedded	xln	medium crystalline
lam	lamina (-tions, -ated)	xtl	crystal

THE FIRST WORD IN THE DESCRIPTION COLUMN OF THE CORE ANALYSIS REPORT DESCRIBES THE ROCK TYPE. FOLLOWING ARE ROCK MODIFIERS IN DECREASING ABUNDANCE AND MISCELLANEOUS DESCRIPTIVE TERMS.

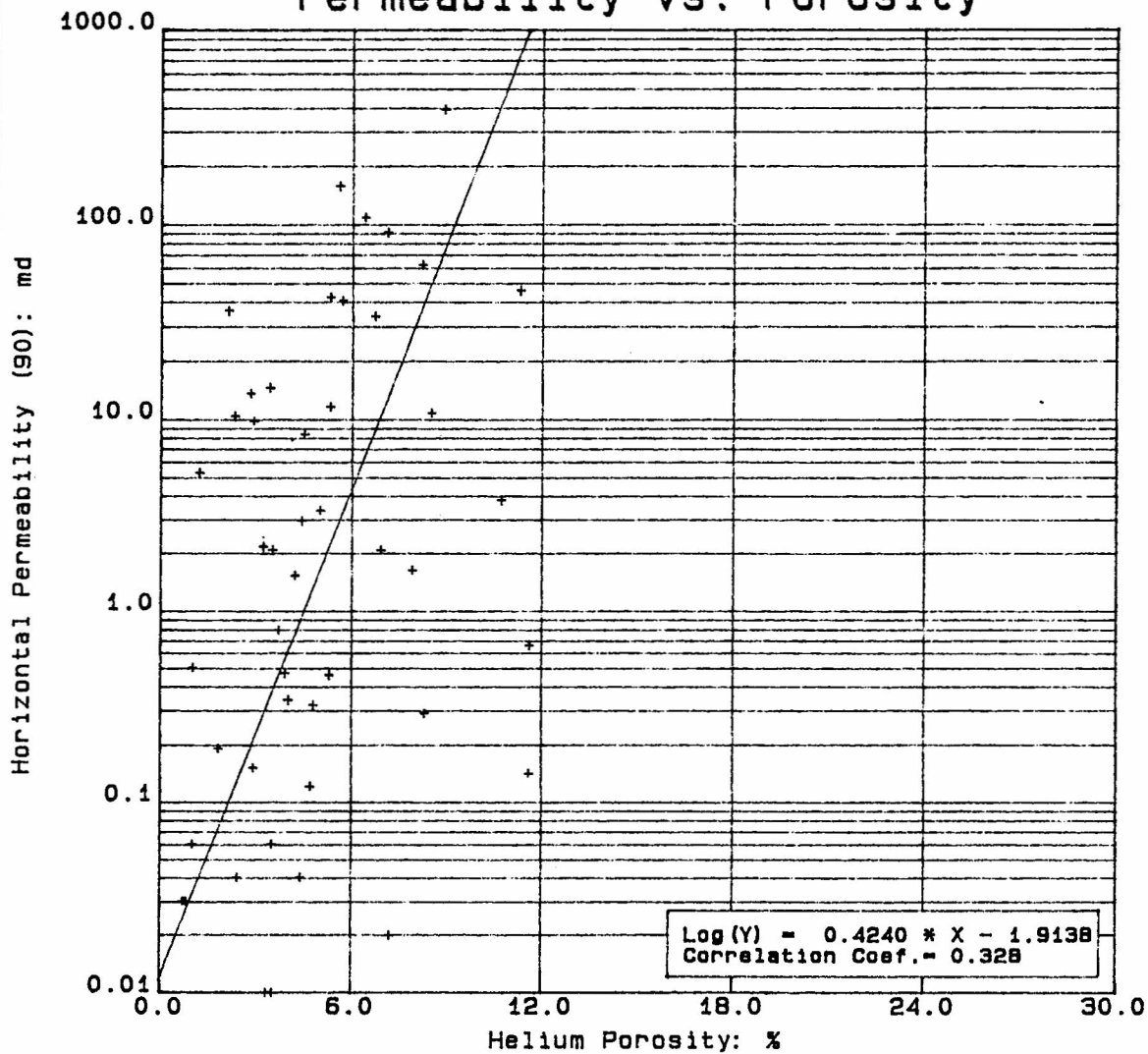
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Permeability vs. Porosity



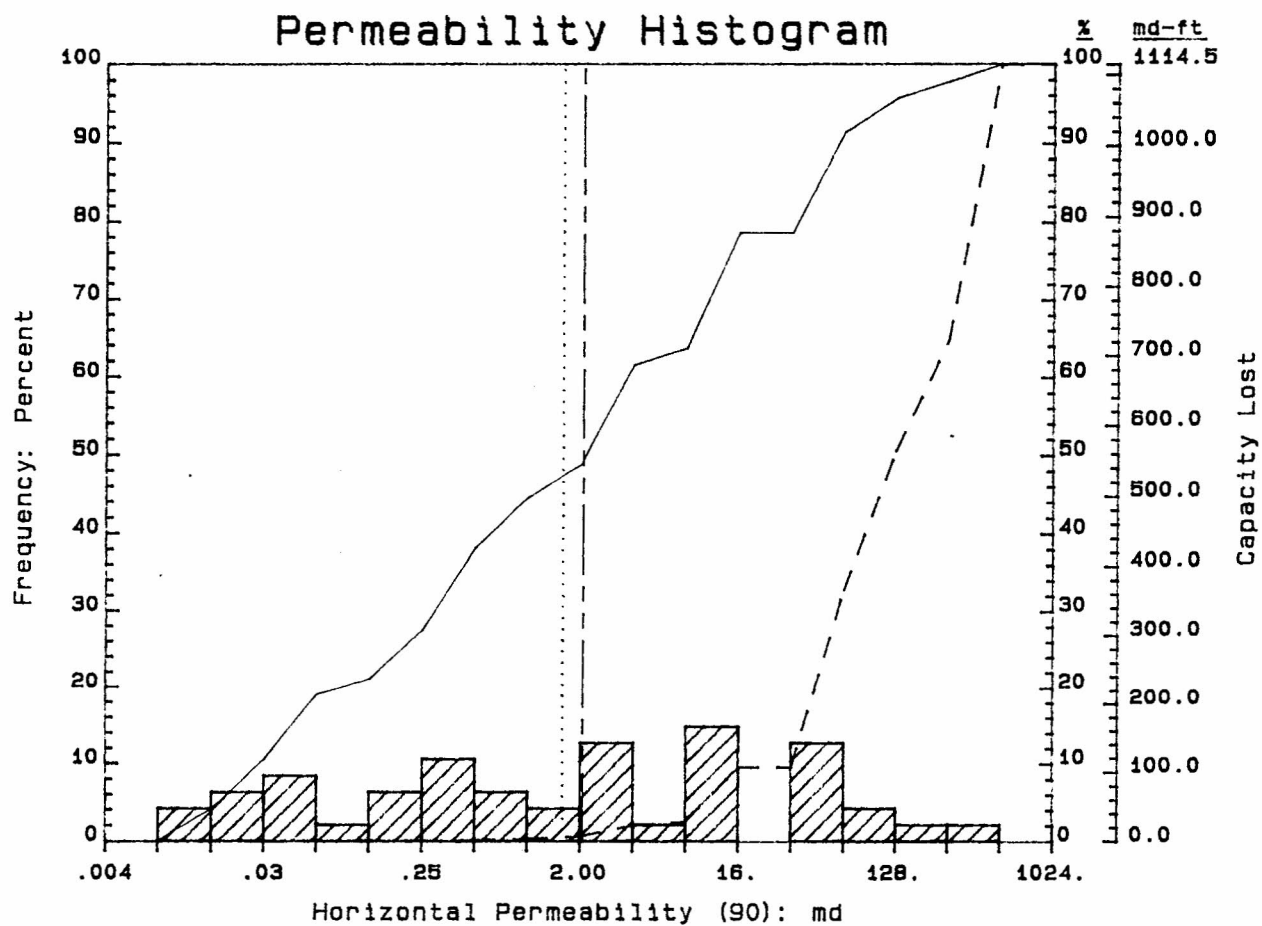
ELK OIL COMPANY
KELLS STATE NO. 1
SOUTH ACME SAN ANDRES FIELD

SAN ANDRES (2130-2190 feet)

Core Laboratories

3-20-93

- LEGEND -
SAN ANDRES



ELK OIL COMPANY
 KELLS STATE NO. 1
 SOUTH ACME SAN ANDRES FIELD
 SAN ANDRES (2130-2190 feet)

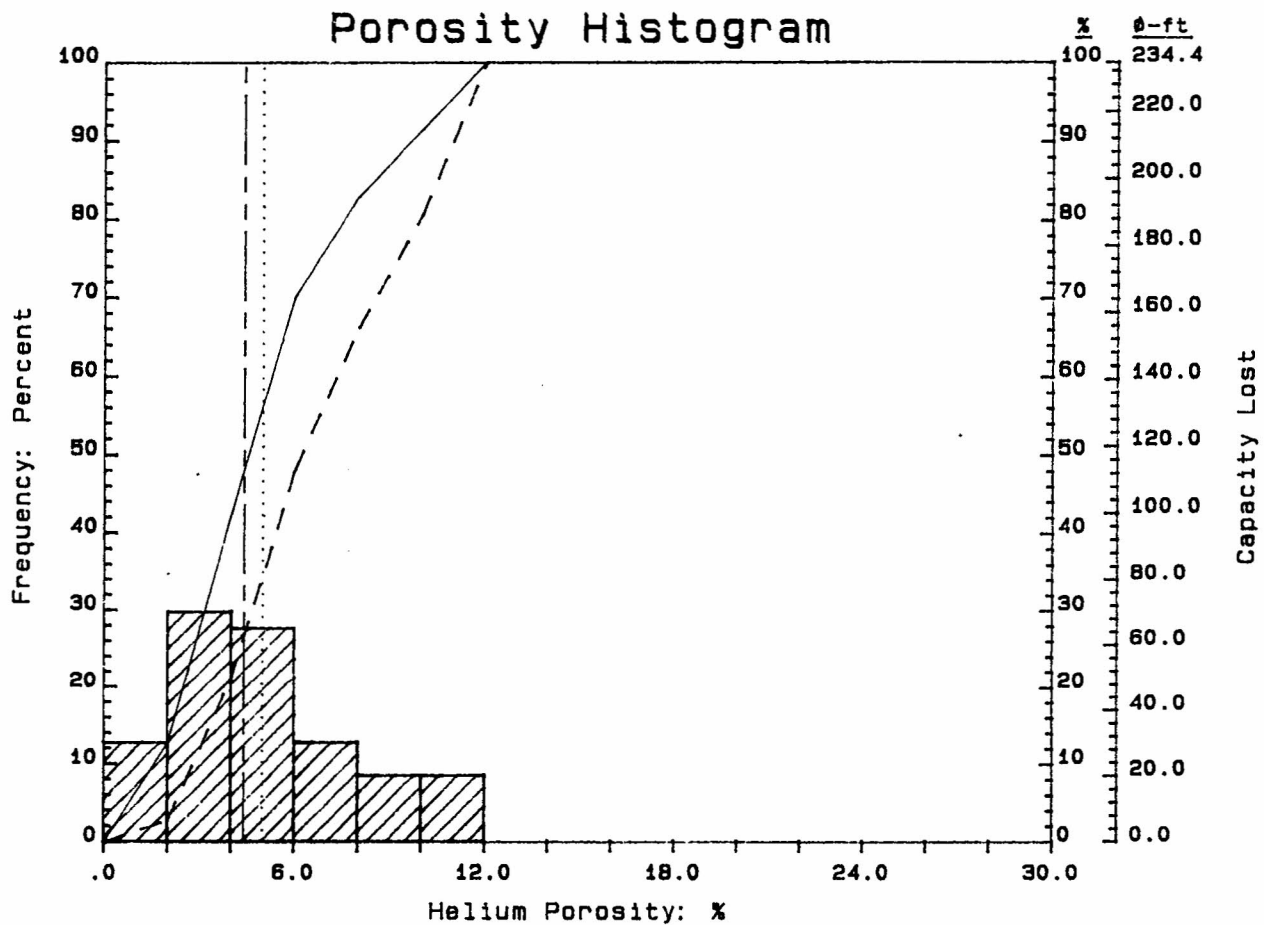
Core Laboratories

3-20-93

- LEGEND -

— Median Value (2.06)
 Geom. Average (1.59)
 — Cumulative Frequency
 - - - Cumulative Capacity Lost

47 Samples



ELK OIL COMPANY
 KELLS STATE NO. 1
 SOUTH ACME SAN ANDRES FIELD

 SAN ANDRES (2130-2190 feet)

Core Laboratories

3-20-93

- LEGEND -

- - Median Value (4.4)
- Arith. Average (5.0)
- Cumulative Frequency
- - - Cumulative Capacity Lost

47 Samples

CORE LABORATORIES

ELK OIL COMPANY
KELLS STATE NO. 1

Field : SOUTH ACME FIELD
Formation : SAN ANDRES

File No.: 57181-16760
Date : 3-20-93

TABLE I

SUMMARY OF CORE DATA

ZONE AND CUTOFF DATA		CHARACTERISTICS REMAINING AFTER CUTOFFS			
ZONE:		ZONE:		PERMEABILITY:	
Identification -----	SAN ANDRES	Number of Samples -----	47	Flow Capacity -----	1114.5 md-ft
Top Depth -----	2130.0 ft	Thickness Represented -	47.0 ft	Arithmetic Average ----	23.7 md
Bottom Depth -----	2190.0 ft			Geometric Average -----	1.59 md
Number of Samples -----	49			Harmonic Average -----	0.10 md
		POROSITY:		Minimum -----	0.01 md
DATA TYPE:		Storage Capacity -----	234.4 ϕ -ft	Maximum -----	392. md
Porosity -----	(HELIUM)	Arithmetic Average ----	5.0 %	Median -----	2.06 md
Permeability -----	(90 DEG) Kair	Minimum -----	0.7 %	Standard Dev. (Geom) --	K.10 $\pm$ 1.227 md
		Maximum -----	11.6 %		
CUTOFFS:		Median -----	4.4 %		
Porosity (Minimum) -----	0.0 %	Standard Deviation ----	$\pm$ 2.9 %	HETEROGENEITY (Permeability):	
Porosity (Maximum) -----	100.0 %			Dykstra-Parsons Var. --	0.964
Permeability (Minimum) ---	0.0100 md	GRAIN DENSITY:		Lorenz Coefficient ----	0.776
Permeability (Maximum) ---	1000. md	Arithmetic Average ----	2.85 gm/cc		
Water Saturation (Maximum)	100.0 %	Minimum -----	2.80 gm/cc	AVERAGE SATURATIONS (Pore Volume):	
Oil Saturation (Minimum) -	0.0 %	Maximum -----	2.89 gm/cc		
Grain Density (Minimum) --	2.00 gm/cc	Median -----	2.85 gm/cc	Oil -----	15.1 %
Grain Density (Maximum) --	3.00 gm/cc	Standard Deviation ----	$\pm$ 0.01 gm/cc	Water -----	31.8 %
Lithology Excluded -----	NONE				

EXAMPLE OF HISTOGRAM USE

TO ASSIST IN SELECTION OF "NET PAY CUTOFF"

Introduction

In most reservoirs, selected lower limits of porosity and permeability are designated as "net pay cutoff". All samples with physical properties that fall below these limits are considered to have a negligible effect on reservoir behavior and are excluded from subsequent calculations. In some cases an appreciable or total loss of oil saturation is observed on the core analysis when permeability or porosity decreases to some low level. When this occurs, the saturation data are helpful in selecting the "cutoff" values. In other cases, oil saturation is found for the complete range of porosity observed, but much of the rock has permeability so low it will contribute only slightly to hydrocarbon flow. In this case, excluding the low permeability rock may mean not counting as net pay a large number of feet of core, but because of its low permeability only a small percentage of the total flow capacity may be lost.

Histogram Use

There is often no clean-cut method to select "net pay cutoff" values. However, one helpful approach that can be applied is to use statistical core data as an aid. These statistical data give you a picture of the overall distribution of porosity and permeability for a quick comparison with other wells. It also allows you to assess (1) how much footage and storage capacity is lost, and (2) how much footage and flow capacity is lost for any selected cutoff.

There is an interrelation of porosity and permeability cutoff values, and one should not be selected without consideration of the effect of the selected value on the other. The tie between the two variables is expressed on the plot of permeability versus porosity which is also attached.

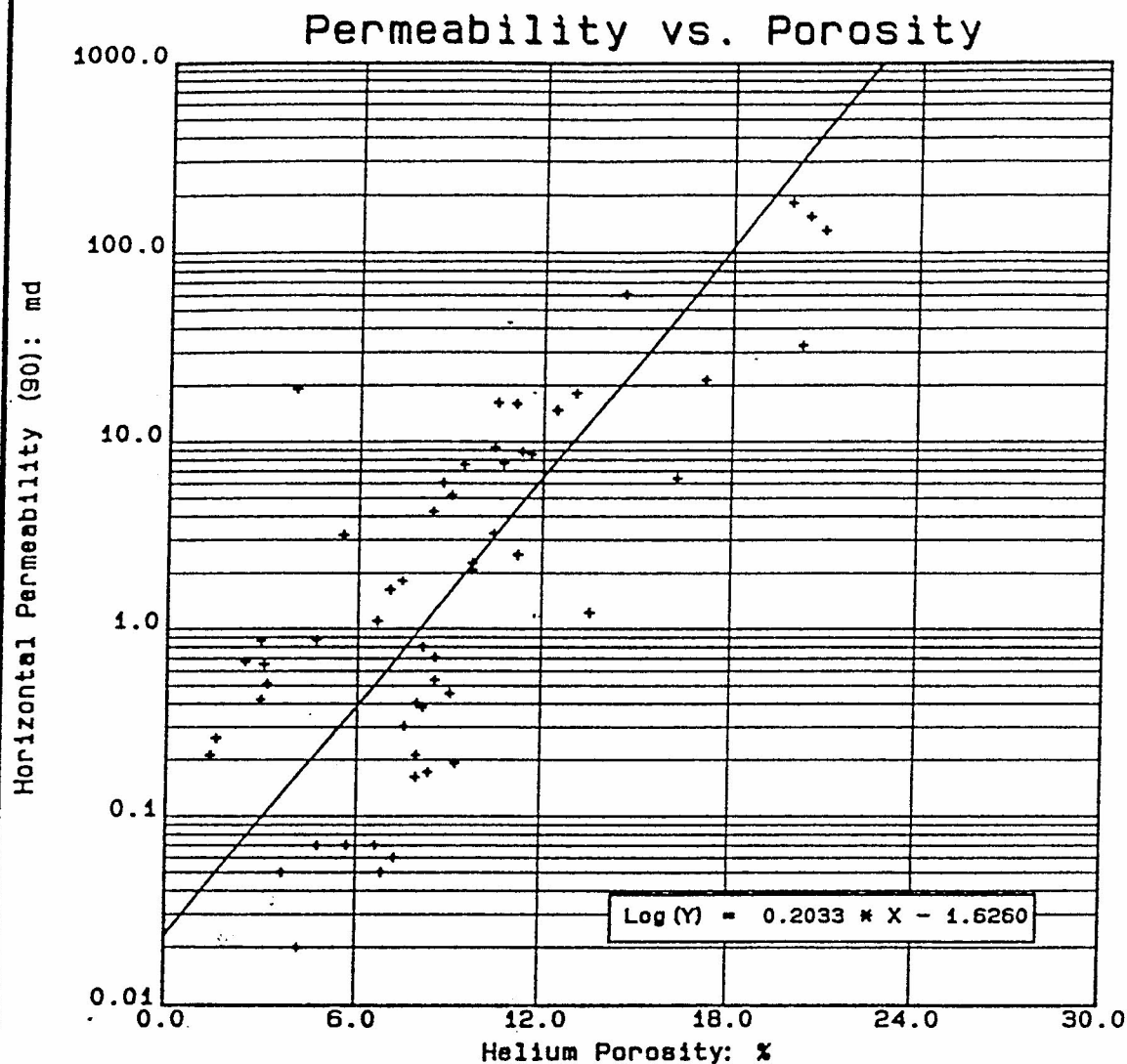
Example

It is necessary to select (often based on experience or knowledge of the area) some lower limit of permeability or porosity as a starting point. Let us assume experience in this area indicates a permeability of 1 millidarcy should be considered as the "net pay cutoff". Entering the permeability histogram with this value, and moving vertically upward to intersect the dashed

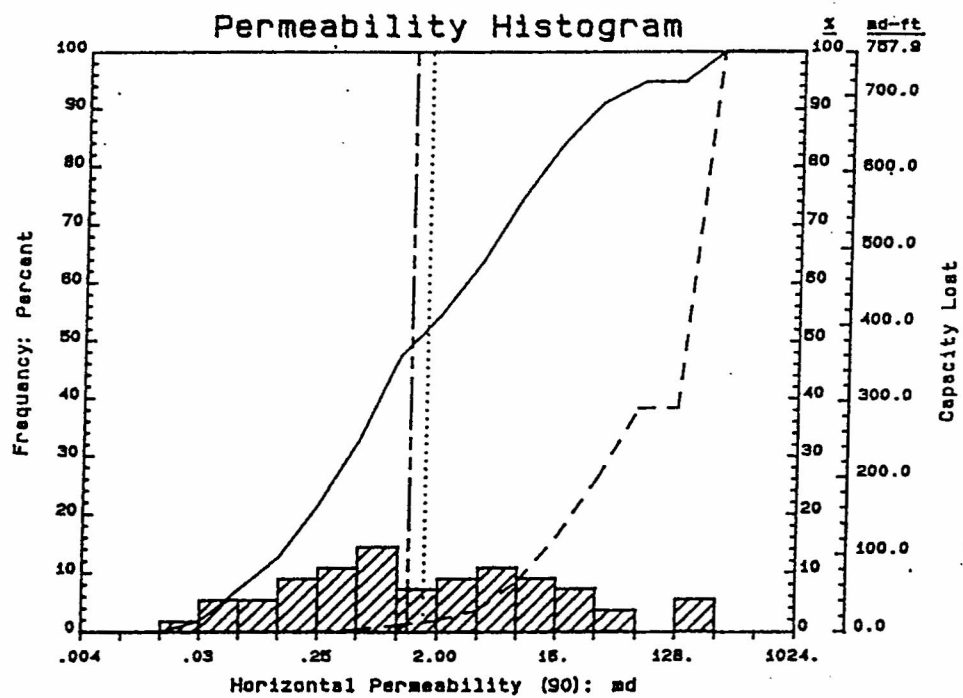
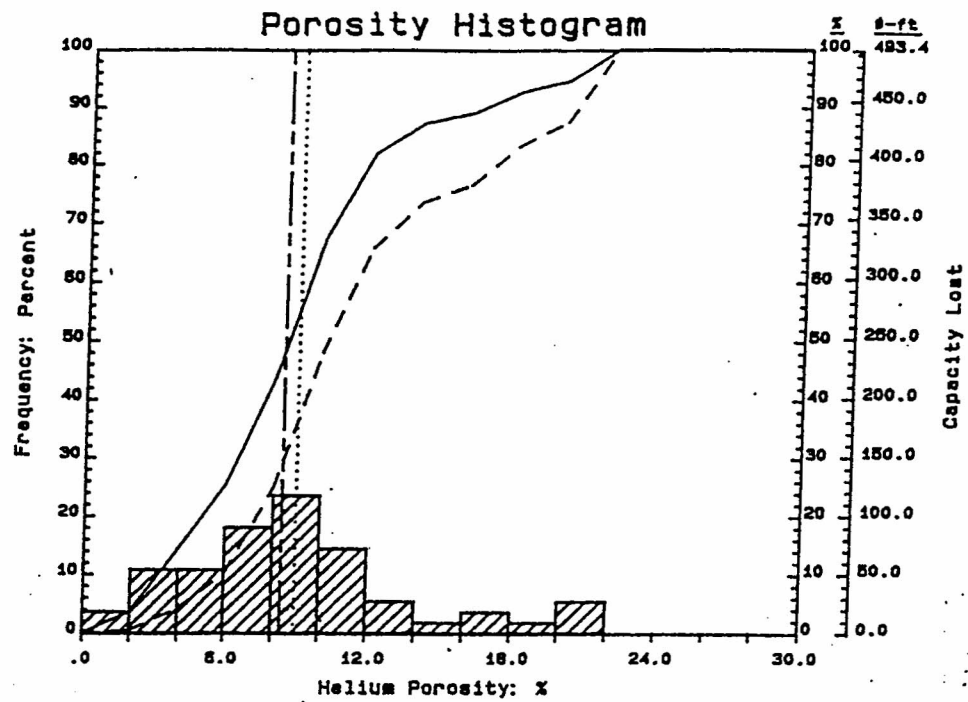
"cumulative capacity lost" line indicates less than 1% of the total flow capacity would be lost by this permeability selection. This sounds good. Continuing vertically upward to intersect the solid "cumulative frequency" line indicates that approximately 45 percent of the total number of samples have one millidarcy permeability or less and would not be counted as net pay. This may be acceptable, but before deciding we must examine the influence of our selection on the storage capacity that will be lost.

Entering the porosity vs. permeability plot at 1 millidarcy furnishes an average porosity of 8%. We return to the histogram plot and enter with a porosity of 8%. Moving vertically upward to intersect the dashed "cumulative capacity lost" curve indicates that with a porosity cutoff of 8%, 24 percent of the total storage capacity would be ignored. Continuing vertically upward to the solid "cumulative frequency" curve indicates that 42 percent of the total number of samples would be discarded. The 24 percent would likely be an excessive loss of storage capacity. This would certainly be excessive if capillary pressure studies indicated that the reservoir water saturation was low (resulting in high oil saturation) in the 8% and less porosity rock, but might be acceptable if the 8 % porosity rock of 1 millidarcy and lower contained a high water saturation.

Study of these plots indicates that a cutoff of 6% porosity might be a more acceptable selection. This cutoff would yield a loss of only 10 % of the total storage capacity, and only 24% of the total footage. Six percent porosity corresponds to a permeability of 0.4 percent millidarcys depending on the drawing of the permeability versus porosity plot. Using 0.4 as the maximum permeability value would result in a cutoff of less than 1 percent of the total flow capacity, and a loss of approximately 25 percent of the total footage. This would likely be a suitable compromise, although the cutoff porosity could be reduced to 4% with little additional loss of storage and flow capacity.



The core analysis permeability vs. porosity plot can be used to relate log porosities to equivalent permeabilities. Also, in conjunction with core analysis histograms, the permeability vs. porosity plot can be used to aid in the evaluation of permeability and porosity cutoffs. Other uses include aiding in reservoir descriptions and selecting ranges for subsequent special core analysis tests.



- LEGEND -

- Median Value —
- Geom. Average
- Cumulative Frequency —
- - - Cumulative Capacity Lost

CORE LABORATORIES

STATISTICAL DATA WORKSHEET

IDENTIFICATION (zone label)	DEPTH TOP feet	DEPTH BOTTOM feet	MIN PHI %	MAX PHI %	MIN Kair md	MAX Kair md	MIN So	MAX Sw	MIN GR DEN	MAX GR DEN
DEFAULT			0	30	0.01	1000	0.0	100.0	2.00	3.00
ZONE A	4525	4650	0	30	0.01	100	8.0	60.0	2.80	2.96

HOW TO FILL OUT WORKSHEET:

For each separate interval on which you want statistical data generated, fill in the appropriate information. For any column which is left blank, the default value listed will be used.

SPECIAL COMMENTS:

SIGNED:

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COMPLETION COREGRAPH

ELK OIL COMPANY
KELLS STATE NO. 1
SOUTH ACME SAN ANDRES FIELD

SAN ANDRES (2130-2190 feet)

Core Laboratories

3-20-93

Vertical Scale
5.00 in = 100.0 ft

Grain Density
gm/cc
2.50 3.00

Total Gamma
API
0 100

Depth
Feet
2100

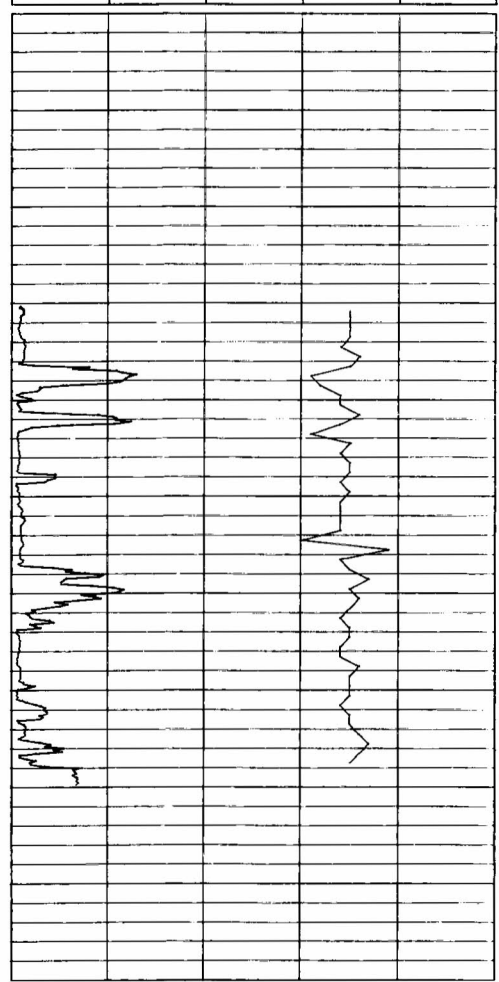
Helium Porosity
%

Horiz K90
md
100 0.01 0

Horiz Kmax
md
0 100 0.01 100

Oil Sat
%

Water Sat
%



2150

2200

